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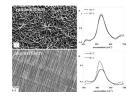


Graphical abstract

Neat and GNPs loaded natural rubber fibers by electrospinning: Manufacturing and characterization

pp. xxx-xxx

Ilaria Cacciotti*, John N. House, Claudia Mazzuca, Manlio Valentini, Francesco Madau, Antonio Palleschi, Paolo Straffi, Francesca Nanni



SEM micrographs and ATR spectra of random and aligned NR based fibers.

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Highlights

Neat and GNPs loaded natural rubber fibers by electrospinning: Manufacturing and characterization

Materials and Design xxx (2015) xxx -xxx

llaria Cacciotti a.b.*, John N. House^c, Claudia Mazzuca^d, Manlio Valentini b.e, Francesco Madau^{b.e}, Antonio Palleschi d, Paolo Straffi c, Francesca Nanni b.e

- ^a University of Rome "Niccolò Cusano", INSTM RU, Via Don Carlo Gnocchi 3, 00166 Rome, Italy
- b Italian Interuniversity Consortium on Materials Science and Technology (INSTM), Italy
- ^c Bridgestone Technical Center Europe, via Fosso del Salceto 13-15, 00128 Castel Romano (Rome), Italy ^d University of Rome "Tor Vergata", Department of Chemical Science and Technology, Via della Ricerca Scientifica 1, 00133 Rome, Italy
- e University of Rome "Tor Vergata", Department of Enterprise Engineering, Via del Politecnico 1, 00133 Rome, Italy
- · Natural rubber (NR) fibrous mats loaded with graphene nanoplatelets were successfully fabricated by electrospinning technique.
- It has been demonstrated that the electrospinning process is able to induce a strong orientation of the polymeric chains.
- The aligned fibers presented remarkably higher dichroic ratio values with respect to the randomly oriented ones.

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Neat and GNPs loaded natural rubber fibers by electrospinning: Manufacturing and characterization

- Ilaria Cacciotti ^{a,b,*}, John N. House ^c, Claudia Mazzuca ^d, Manlio Valentini ^{b,e}, Francesco Madau ^{b,e}, Antonio Palleschi ^d, Paolo Straffi ^c, Francesca Nanni ^{b,e}
 - ^a University of Rome "Niccolò Cusano", INSTM RU, Via Don Carlo Gnocchi 3, 00166 Rome, Italy
 - ^b Italian Interuniversity Consortium on Materials Science and Technology (INSTM), Italy
 - ^c Bridgestone Technical Center Europe, via Fosso del Salceto 13-15, 00128 Castel Romano (Rome), Italy
 - d University of Rome "Tor Vergata", Department of Chemical Science and Technology, Via della Ricerca Scientifica 1, 00133 Rome, Italy
 - ^e University of Rome "Tor Vergata", Department of Enterprise Engineering, Via del Politecnico 1, 00133 Rome, Italy

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- Electrospinning 22 23
 - FTIR (polarized ATR)

ABSTRACT

The interest towards natural rubber (NR) is progressively increasing due to its sustainable production and re- 24 markable mechanical properties, presenting a wide application range in the automotive industry and civil engineering. In this paper we report, for the first time, the use of electrospinning technique to produce neat and 26 graphene nanoplatelets (GNPs, 1 wt.%) loaded natural rubber fibers. Both randomly distributed and aligned fibers 27 (average diameter size ~1 µm) mats were obtained, resulting uniform and defect-free. A detailed characterization 28 of these fibers is reported, including field emission-scanning electron microscopy (FEG-SEM), X-Ray diffraction 29 (XRD) and infrared spectroscopy (FTIR-ATR) techniques. It has been demonstrated that the electrospinning pro- 30 cess is able to induce a strong orientation of the polymeric chains in the case of aligned fibers, with respect to the 31randomly oriented fibers and solvent cast films.

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1. Introduction

Among the fiber production techniques, electrospinning is a user friendly, versatile and low-cost method, which allows to manufacture different materials (e.g. polymers, ceramics, metals, composites) with diameters ranging from nanometers to micrometers and large surface area-to-volume ratio [1-6]. Only few attempts of electrospinning elastomers/rubbers are currently reported in literature, due to their poor spinning ability in conventional solvent systems, which is related to their viscoelastic behavior at room temperature and fiber formation mechanism during electrospinning. For example, only fibers based on polybutadiene rubber (BR) [7–8], synthethic cis-1,4-polyisoprene [9], blends of natural rubber (NR)/acrylonitrile butadiene styrene (ABS) [10] and of NR/polycaprolactone (PCL) [11] were successfully obtained by electrospinning technique. To the best of our knowledge, actually none of the papers reported in literature deals with sole natural rubber.

Among the elastomers, natural rubber attracts a lot of attention, due to its outstanding performance properties such as high elasticity, resilience and good fatigue resistance [12] and its application for the manufacture of more than 40,000 consumer products, including tires, wires,

E-mail address: ilaria.cacciotti@unicusano.it (I. Cacciotti).

latex products, footwear, medical devices and sport components [13, 57 14]. In this framework, the present work reported a first attempt to de- 58 velop neat and graphene nanoplatelets (GNPs) loaded natural rubber fi- 59 bers by this technique. The application of electrospinning technique to 60 produce natural rubber based fibers was achieved using the dry rubber 61 (DR) extracted from natural rubber latex (NRL). The extracted DR was 62 dissolved in chloroform to enhance its spinning ability. The GNPs were 63 chosen and selected as conductive fillers in order to evaluate their influ- 64 ence on the microstructure of the obtained fibrous membranes. In this 65 contest, several micro- and nano-sized conductive fillers, such as carbon 66 black (CB), metallic powders (e.g. silver and copper), and carbon nano- 67 tubes (CNTs), are commonly used due to their light weight, high flexi- 68 bility and ability to absorb mechanical shocks in order to prepare 69 natural rubber composites [15], for applications in the fields of electro- 70 magnetic interference shielding, self-regulated heating, package mate- 71 rial and pressure sensors [16]. It has been demonstrated that the filler 72 properties, in terms of particle size, surface area, aggregate structure, 73 surface activity and conductivity, can strongly influence the characteris- 74 tics of the final composite [15]. The electrospinning set-up to produce 75 both randomly distributed and aligned fibers was accomplished by 76 properly tuning process parameters, in terms of applied voltage, nee-77 dle-target distance, collector type (i.e. fixed or rotating, respectively). 78 Furthermore, the crystallization and/or macromolecular orientation of 79 the natural rubber chains in the produced randomly distributed and 80

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^{*} Corresponding author at: University of Rome "Niccolò Cusano", INSTM-RU, Via Don Carlo Gnocchi 3, 00166 Rome, Italy.

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aligned fibers were investigated. Morphology thermal behavior, microstructure and the orientation of the polymeric chains were investigated by scanning electron microscopy (FEG-SEM), simultaneous thermogravimetric and differential analyses (TG-DTA), X-Ray diffraction (XRD) and infrared spectroscopy (ATR-IR), respectively.

2. Experimental

2.1. Preparation of dry rubber based solutions and suspensions

The natural rubber latex (R1 International PTE LTD) consisted in a colloidal suspension of cis-polyisoprene in natural rubber serum preserved with ca. 0.7% of ammonia and a mixture of lauric acid, tetramethyl thiuram disulfide and zinc oxide. The pH value of the suspension was 10 and the density at 20°C of 0.998 g/cm³. Firstly the latex was poured in a Petri dish and afterwards completely covered with acetone (Carlo Erba Reagents), in order to favor the evaporation of the emulsion's volatile components. This process was carried out until the final weight of the compound was 40% less than the initial weight (i.e. dry rubber). The obtained DR was then dissolved in chloroform (CHCl₃, 99%, Carlo Erba Reagents) at 1 and 2% w/w under constant magnetic stirring for three days. Hybrid suspensions based on rubber and graphene nanoplatelets (GNPs, Cometox, average thickness 15 nm, typical surface area $50 \div 80 \text{ m}^2/\text{g}$, as reported in the datasheet) were also prepared. The GNPs dispersion was performed in chloroform by sonication (Sonics Vibracell CV33) for 1 h at 30% amplitude in an ice bath, followed by centrifugation (Thermo Electron Corporation ALC 4218) for 1 h at 3000 rpm and further sonication for 1 h at 30% amplitude. Afterwards, the dry rubber was added to the GNPs suspension in order to obtain a 2% w/w rubber concentration in chloroform and a 1% w/w concentration of GNPs compared to the dry latex content. The viscosity of the as received latex and all the prepared solutions/suspensions was measured at 25 °C using a dynamic viscometer (Brookfield DV-II+, Middleboro, MA, ÛSA), equipped with a SC4-21 spindle, and the conductivity measurements of the different samples were carried out with an electrical conductimeter (CDM230, Analitica De Mori, Italy).

2.2. Fabrication of neat and hybrid fibrous mats by electrospinning

The prepared solutions and suspensions were poured in a glass syringe (Socorex, Switzerland) equipped with a 20 G needle, fixed in a digitally controlled syringe pump (KD Scientific, MA, USA) and electrospun in air at room temperature in the following conditions: applied voltage 16 kV, feed rate 0.5 ml/h, needle-target (N-T) distance 10-18 cm and 12-16 cm for fixed and rotating targets, respectively. In Table 1 the samples designation and the related electrospinning parameters are summarized. Finally, as reference, neat and hybrid films were prepared by solvent casting technique, pouring the prepared solutions/suspensions in Petri dishes and left to dry under the fume hood until the solvent was completely evaporated. Furthermore the same procedure was adopted to prepare neat latex films starting from the as-purchased solution, with and without the acetone addition (i.e. dry rubber w acetone and dry rubber w/o acetone, respectively).

2.3. Characterization of neat and hybrid fibrous mats by electrospinning

The morphology of all samples was investigated by means of Scanning Electron Microscopy (FEG-SEM, Cambridge Leo Supra 35). The average fiber size was determined from SEM micrographs by means of Image J (NIH) software. X-ray diffraction analyses (XRD, Philips X'Pert) were performed in the following conditions: CuK $\alpha \lambda = 1.5402^{-}\text{Å}$, 20 range 5°-90°, step size 0.020°, time per step 2 s. Thermogravimetric measurements (TG-DTA) were carried out in nitrogen atmosphere (flow 80 cm³/min) by simultaneous thermogravimetric and differential thermal analysis (TG-DTA, Netzsch STA 409), in the following conditions: sample weight about 60 mg, temperature range 20–1250 °C, heating

Designation of the electrospun neat and hybrid fibers and used process parameters (all the t1.2samples were electrospun using a feed rate of 0.5 ml/h and a voltage of 16 kV).

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t1.3

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ample	Latex concentration (wt.%)	GNPs filler concentration (wt.%)	Target type	Needle_target distance (cm)
R1:ES-F	1		Fixed	10
				12
DR2:ES-X	2	Ţ.	Fixed	10
				12
				14
				16
				18
			Rotating	10
				12
				14
NP/DR2:	2	1	Fixed	14
ES-X				16
				18
			Rotating	14
				16
				18

ES = electrospinning. t1.21 $X = \hat{F}$ or R if the fixed or rotating collector was used, respectively.

rate 5 °C/min. In order to characterize the natural rubber components, 140 FTIR spectra were acquired on a Thermo-Nicolet (mod. Nexus 670) in- 141 strument (Thermo Scientific Inc., Madison WI), equipped with an atten- 142 uated total reflectance (ATR) ZnSe cell for measurement in the 4000- 143 750 cm^{-1} region, at a resolution of 4 cm⁻¹. Spectra were collected by 144 placing and pressing the samples into contact with the ATR cell. A 145 total of 256 scans were collected for each sample. In addition, polarized 146 ATR-IR spectra were acquired on all samples in order to study the mo- 147 lecular orientation of polymer chains due to the polymer processing 148 technique. To achieve a complete analysis of the samples, four separate 149 spectra were acquired using polarized light at 0° and 90° with respect to 150 the sample's plane and positioning the samples longitudinally (L) and 151 transversally (T) to the direction of the stress applied during the processing. Thus the dichroic ratio was evaluated by the ratio between 153 peak intensities in two different configurations, as expressed with the 154 followings equations:

$$R_{X}\left(\frac{\alpha}{\beta}\right) = \left(\frac{A(\alpha)}{A(\beta)}\right)_{X} \tag{1}$$
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$$R_{\alpha} \left(\frac{X}{Y} \right) = \left(\frac{A(X)}{A(Y)} \right)_{\alpha} \tag{2}$$

where X and Y are the longitudinal and transversal configurations and α and β the polarizer orientations [17]. In all cases the peak at 161 2960 cm⁻¹, related to the CH₃ asymmetric stretching, was used as 162 non-dichroic peak (i.e. as reference), since it presents a unitary dichroic 163 ratio independently of the polymer structure. While the peaks at 164 1367 cm $^{-1}$ (CH₃ deformation) and at 837 cm $^{-1}$ (= CH out of plane 165 bending) were selected to calculate the dichroic ratio (R) in all the selected configurations, in order to investigate the orientation of the macromolecular chains of the cis-1,4-polyisoprene [18,19]. 168

3. Results and discussion

3.1. Characterization of dry rubber

The dry rubber used for the preparation of the solutions/suspensions 171 was characterized by XRD analysis, thermal analysis and ATR-IR spec- 172 troscopy, before and after the acetone treatment, in order to evaluate 173 the preservation of the non-rubber components (such as proteins and 174 phospholipids) in the treated DR. In fact, it is well known that the 175

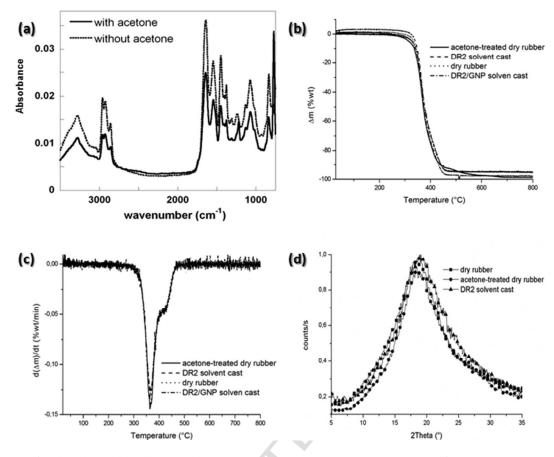


Fig. 1. (a) ATR-IR spectra of the dry rubber with (dotted line) and without (continuous line) acetone treatment. Spectra are staggered for clarity; (b) TG and (c) DTG curves of the dry rubber, acetone-treated dry rubber, neat and GNP loaded solvent cast DR2 films; (d) XRD diffraction pattern of the acetone treated and no-treated dry rubber and of the DR2 solvent cast film.

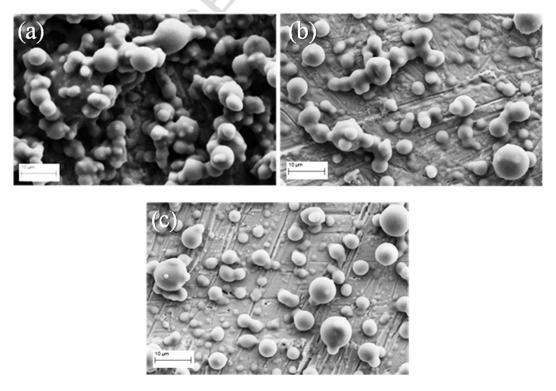


Fig. 2. SEM micrographs of the as received latex deposited at different needle–target distances (applied voltage 16 kV, feed rate 0,5 ml/h): (a) 10 cm, (b) 14 cm and (c) 16 cm.

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Table 2Viscosity and conductivity values of the chloroform, as received latex and prepared solutions/suspensions.

Sample	Conductivity (µS/cm ²)	Viscosity_(cP)		
		@ 20_rpm	@ 50 __ rpm	@ 100_rpm
Chloroform	0.011 ± 0.002		-	-
As received latex	7.2 ± 1.3	41.2 ± 0.1	30.6 ± 0.2	31.5 ± 0.2
DR1	0.011 ± 0.002	64.5 ± 0.7	61.0 ± 0.1	57.5 ± 0.7
DR2	0.008 ± 0.001	86.6 ± 0.1	76.7 ± 0.1	66.4 ± 0.3
GNP/DR2	0.013 ± 0.003	144 + 1	116 + 1	96.1 ± 0.2

presence of these components may enhance and promote the rubber crystallization [20]. Comparable ATR-IR spectra were acquired before and after the treatment of the latex (Fig. 1a), detecting the typical natural rubber functional groups [21] and the vibrational modes of the nonrubber components (i.e. proteins and phospholipids) at 1542 cm⁻¹, 1240 cm⁻¹ and 1740 cm⁻¹, imputable to the N-H bending, the O-P-O asymmetric stretching and the C=O stretching of the phospholipids, respectively. Thus, it is possible to state that the acetone treatment did not influence and alter the presence of proteins and phospholipids. These results were confirmed by both thermogravimetric and X-ray diffraction analyses, proving that the selected treatment to obtain dry rubber was appropriate since all chemical characteristics of untreated rubber were maintained (Fig. 1b-d). Moreover it was verified through the same characterization techniques that the DR dissolution process in chloroform, in the case of the solutions prepared for the fiber preparation, did not induce any compositional modification. In details, in Fig. 1b-c the TG and DTG curves of the dry rubber samples with and without acetone treatment and of the neat and hybrid 2 wt.% DR solvent cast films are compared, presenting the same general shape. In all cases it is evident that the thermal degradation of the natural rubber is mostly a one-stage process [22], ranging the decomposition from approximately 300 °C to 450 °C with a mass loss of about 95%. The primary degradation peak in the DTG curves was ascribable to the thermal decomposition of the natural rubber into monomers, dimers and trimers, whereas the small shoulder curve at around 420_°C can be asso-200 ciated to the higher temperature degradation of crosslinked and 201 cyclized networks [23]. XRD analysis of acetone treated and no-202 treated dry rubber and of the solvent cast film obtained from the chlo-203 roform solution showed the typical diffraction spectrum of this material 204 in the amorphous phase, which is characterized by a broad peak at 20–205 18° [24] (Fig. 1d). In fact, the isoprene molecules are coupled to form 206 an irregular amorphous rubbery structure that cannot crystallize 207 under normal conditions [25,26], but requires the application of a strain 208 ("strain-induced crystallization", SIC). In conclusion, all the collected ex-209 perimental data demonstrate that chloroform dissolution, as well as ac-210 etone treatment, did not induce any significant change to the rubber 211 properties.

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3.2. Morphology of the produced electrospun mats

The main technical issue was to find the optimum balance of solu- 214 tion/suspension viscosity and conductivity to allow the spinning of 215 neat and GNP loaded NR solutions/suspensions. Based on the analysis 216 and taking into account pure latex as reference, 2% w/w DR in chloro- 217 form and 1% w GNP with respect to DR were found to be a suitable com- 218 bination in terms of conductivity and viscosity increase. The former was 219 set up, testing different weight percentages in order to improve the 220 spinning ability and fiber dimension control. SEM analysis confirmed 221 the trend evidenced by Fong et al. [27] between viscosity and fiber qual- 222 ity: the processing is remarkably influenced by solution viscosity and for 223 values below 60 cP spinnability is hindered. In fact, as received latex 224 showed spraying behavior (Fig. 2), due to its low viscosity (i.e. 40 cP, 225 Table 2), while increasing viscosity to 60 cP (i.e. DR1 solution) allowed 226 fiber formation, although the fiber quality was very poor: fibers were 227 not uniform, characterized by numerous and diffuse beads and imper- 228 fections, seemed to be melted together and tangled on each other 229 (Fig. 3), owing to a not complete solvent evaporation during the flight 230 from the needle orifice to the target. Furthermore, an increase of nee- 231 dle-target distances leaded to no spinnability. On the other hand, vis- 232 cosity greater than 80 cP (DR2 solution) showed good spinnability 233

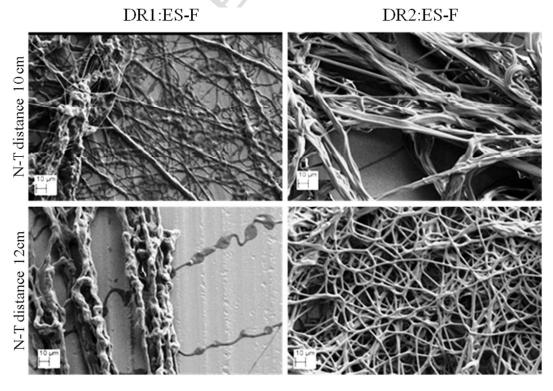


Fig. 3. SEM micrographs of the DR1:ES-F and DR2:ES-F fibers deposited at different needle-target (N-T) distances (applied voltage 16 kV, feed rate 0,5 ml/h).

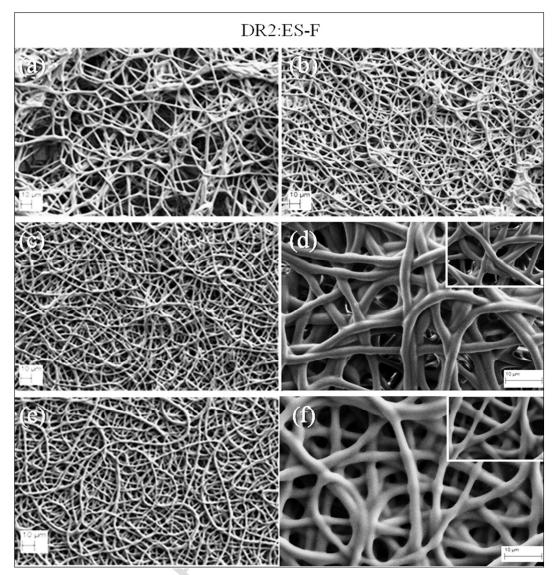


Fig. 4. SEM micrographs of the DR2:ES-F fibers deposited at different needle_target (N_T) distances (applied voltage 16 kV, feed rate 0,5 ml/h): (a) 12 cm, (b) 14 cm, (c_d) 16 cm, (e_f) 18 cm.

and uniform, homogeneous and defect-free fibers were obtained, independently from the needle-collector distance (Fig. 4). The best morphological characteristics were obtained selecting needle-target distances of 16 cm and 18 cm (Fig. 4). Indeed, increasing the needle-target

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Table 3 Average diameters of neat DR2 and hybrid GNP/DR2 electrospun fibers (all values are expressed as mean values \pm standard deviation (SD)).

Sample	N-T distance (cm)	Fiber diameter (µm)
DR2:ES-F	10	1.5 ± 0.2
	12	1.4 ± 0.2
	14	1.1 ± 0.1
	16	1.0 ± 0.1
	18	0.9 ± 0.2
DR2:ES-R	10	1.2 ± 0.2
	12	1.1 ± 0.1
	14	1.1 ± 0.4
GNP/DR2:ES-F	14	1.3 ± 0.2
	16	1.3 ± 0.2
	18	1.2 ± 0.2
GNP/DR2:ES-R	14	1.3 ± 0.3
	16	1.1 ± 0.2
	18	1.2 ± 0.3

distance allowed to obtain more uniform and homogeneous fibers, 238 due to the better solvent evaporation and proper flight time. Moreover, 239 high magnification micrographs reveal smooth surfaces without macro- 240 scopic defects (Fig. 4) and a reduction of fiber diameter increasing the 241 needle-target distance (Table 3), in agreement with literature [27,28]. 242 Fig. 5 shows a comparison between electrospun fibers from GNP/DR2 243 suspension at different needle-target distances (i.e. 14–18 cm). All the 244 obtained GNP/DR2:ES-F samples consisted of uniform and bead-free fi- 245 bers which were tangled on each other and showed some melted areas. 246 This phenomenon seemed to decrease with increasing N-T distance. 247 The high magnification SEM images evidenced a uniform dispersion 248 and distribution of the filler within the fibers (Fig. 5). The maximum di- 249 mension of the filler was about $1 \mu m^2$, whereas smaller aggregates were 250 also observed. It is worth to notice that the hybrid GNP/DR fibers pre- 251 sented a rough surface, whereas the neat fibers were smooth. In a sec- 252 ond step a rotating collector was employed in order to analyze the 253 influence on fiber dimension and morphology and to try to induce poly- 254 mer chains orientation. Concerning the fibers spun from the DR2 solu- 255 tions on the rotating drum, the fiber quality is comparable to previous 256 ones, in terms of both fiber dimension (Table 3) and surface roughness 257 (Fig. 6), being all fibers very smooth. The DR2 fibers obtained varying 258 the needle-target distance in the range 10-14 cm are compared in 259

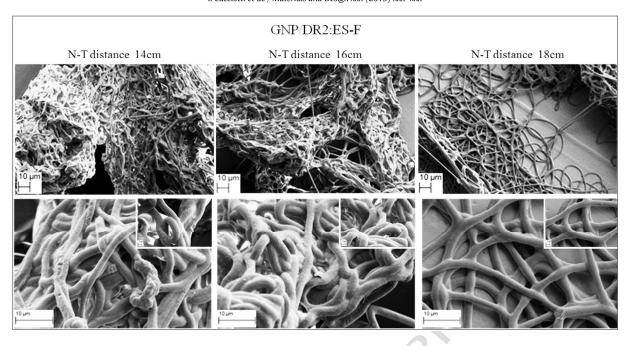


Fig. 5. SEM micrographs of the GNP/DR2:ES-F fibers deposited on a fixed collector at different needle—target (N_T) distances (i.e. 14 cm, 16 cm and 18 cm) (applied voltage 16 kV, feed rate 0.5 ml/h). In the inserts high magnification SEM micrographs are reported.

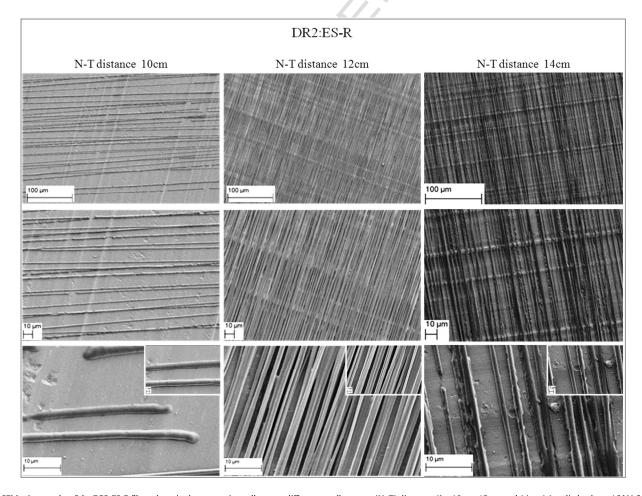


Fig. 6. SEM micrographs of the DR2:ES-R fibers deposited on a rotating collector at different needle–target (N–T) distances (i.e. 10 cm, 12 cm and 14 cm) (applied voltage 16 kV, feed rate 0,5 ml/h).

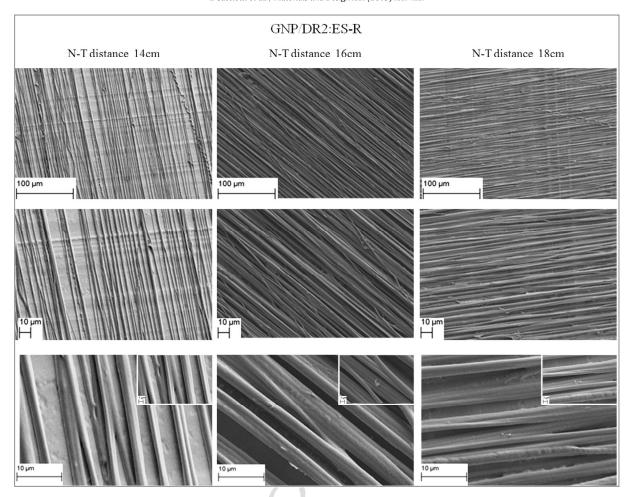


Fig. 7. SEM micrographs of the GNP/DR2:ES-R fibers deposited on a rotating collector at different needle-target (N-T) distances (i.e. 14 cm, 16 cm and 18 cm) (applied voltage 16 kV, feed rate 0,5 ml/h).

Fig. 6. The fibers deposited at a distance of 10 cm were uniform, smooth and bead-free, but spaced out and broken in many points and not perfectly aligned. In fact, since the elastomers/rubbers have glass transition temperatures lower than room temperature, the macromolecules chain segments are able to move and to rearrange their conformations in electrospun nanofibers. The molecular movement/relaxation usually occurs when the stretching force (particularly during the bending instability [28]) no longer exists, and is driven by entropy increase. Thus the breakage/conglutination of nanofibers can be observed with prolonging the storage time. This would be imputable to the characteristics of cis-1.4-polyisoprene, such as weak interaction between molecular chains, strong chain entanglement originating from rather flexible chain and elasticity, which may cause shrinking after release of Coulomb force [9]. On the contrary fibers spun at a distance of 12 cm were highly aligned, uniform, bead-free and did not present any type of morphological imperfection. The fibers deposited at a distance of 14 cm were very similar to the ones obtained at 10 cm, showing high alignment, but also poor uniformity and the presence of surface defects. Thus, the sample deposited at 12 cm presented the best morphological characteristics and was subjected to the other characterizations. Comparing the diameters of the fibers deposited on the fixed and rotating targets at the same needle-collector distance (Table 3), it is evident that the kind of target does not play a significant influence on the final fiber diameter. This experimental evidence could be due to the limited speed of the rotating collector. As a matter of fact, since the fibers are composed of an elastomer, if they were stressed with a significant rotational force, the rubbery material would have been stretched in the rotational direction causing shrinkage in the other directions. It cannot be excluded that a higher

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rotational speed would have promoted this effect. The analysis of GNP 288 loaded aligned fiber reveals the absence of beads, while their alignment 289 is influenced by the selected needle—target distance (Fig. 7). Indeed, the 290 fibers spun at 14 cm distance were neither highly aligned nor very uniphorm and seemed melted together, as evident in the high magnification 292 micrographs. On the other hand, selecting the distance at 16 cm and 293 to induced an improvement of the alignment and avoided the occurrence of melting phenomena. However, the uniformity of these ficulty bers was not excellent, especially at 18 cm, revealing some surface 296 imperfections, as evident in the high magnification micrographs.

The presence of the filler was detected in the high magnification 298 SEM micrographs, revealing that in some cases, it was oriented in the di- 299 rection of the fiber (Fig. 7). This effect is due to the anisotropic conductivity properties of the GNPs, which are therefore oriented in the 301 direction where the conduction is favored [2]. The reported diameter 302 size values reveal a slight decrement of the fiber diameter with the N- $\,$ 303 T distance (Table 3). Furthermore, the collector type, fixed or rotating, 304 did not exercise any significant influence on fiber diameter, obtaining 305 comparable values under the same processing parameters. As men- 306 tioned previously this could be due to the limited rotating speed of 307 the rotating drum. A comparison between the diameters of the fibers 308 obtained spinning the DR2 solution and the GNP/DR2 suspension for 309 N-T distances of 14 cm, 16 cm and 18 cm provided interesting results. 310 Indeed, the hybrid fibers were slightly thicker than the related neat 311 ones. This phenomenon is strictly correlated to the starting solution 312 properties. As reported in literature, the solution properties, in terms 313 of conductivity and viscosity, play contrasting effects on fiber final di- 314 ameter. An increase in the conductivity of the solution brings to the 315 316 317

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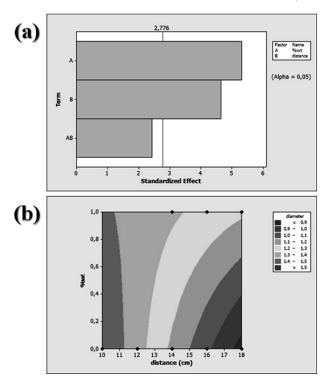


Fig. 8. (a) Pareto chart of standardized effect and (b) contour plot of the response surface related to the influence of the needle_target distance and the filler amount on the resultant fiber average diameter.

formation of thinner fibers, while an increment in the viscosity increases fibers final diameter [29–31].

The values of measured diameters suggest that, even if the addition of GNP to the DR2 solution increases both the conductivity and the viscosity, the increment of viscosity exercises a greater effect on fiber diameter than the increment of conductivity. Based on these results, we can state that viscosity is the main controlling factor of the electrospinning process since neat latex solutions showed spinnability even presenting low conductivity values, and GNP filled fibers were characterized by bigger diameter, despite higher conductivity of the related suspensions. Therefore, a semiempirical correlation between the major experimental parameters and the diameters of electrospun fibers was attempted. Based on literature [27] and experimental experience, two parameters were chosen as input data: one concerning the spinning solution/suspension (i.e. presence of filler which significantly alters the solution/suspension viscosity and conductivity) and the other the

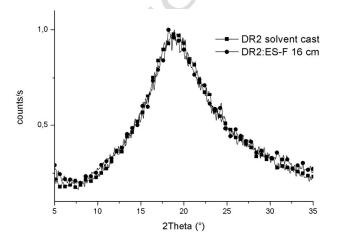


Fig. 9. Comparison of XRD spectra of DR2 solvent cast film and DR2:ES-F fiber mat.

experimental set-up (needle_target distance). Experimental values of 332 DR2 e DR2/GNP samples were used (Table 3). The best fitting matheamatical model for the found experimental data is: 334

$$d = 0.63 \text{ wt.} \% + 0.080 \text{ distance} + 0.055 \cdot (\text{distance} \cdot \text{wt.} \%) + 2.3.$$

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where 'd' is the fiber average diameter (expressed in µm), 'distance' 338 the needle_target distance (expressed in cm), wt.% the filler amount in 339 weight percentage. Considering the related Pareto chart (Fig. 8a) and 340 contour plot of fiber average diameter in function of the two considered 341 parameters (Fig. 8b), it is evident that both the filler amount (A) and the 342 needle_target distance (B) can exercise significant effects on the average diameter of the produced fibers, with a confidence higher than 344 95%. On the other hand, the interaction factor (AB) does not statistically play a remarkable influence on the average diameter of the electrospun 346 fibers, presenting a confidence of 95%.

The regression is in accordance with the physic of the process, since 348 it can be assumed that increasing the distance between needle and 349 target allows higher shrinkage of the fibers as well as the presence of 350 the filler somehow hinders it.

3.3. Microstructural organization and orientation of polymeric chains

The electrospun mats were analyzed through XRD and ATR-IR in order to investigate the microstructural organization and orientation 354 of the polymeric chains in the fibers. As regards XRD results, in all 355 cases, a single broad peak at 18°, typical of the natural rubber, was detected and presented the characteristic shape of the amorphous NR 357 (Fig. 9). Some authors [32] reported contradictory data, stating that 358 the electrospinning process favors the crystallization in polymers with 359 low $T_g \approx 60\,^{\circ}\text{C}$, such as polyesters. However, the acquired spectra 360 showed no evidence of material crystallinity. It is possible to address 361 the lack of crystallinity neither to the poor stretching after spinning 362 nor to the low amount of dry rubber content in the spinning solution. 363

The preferential orientation of the polymeric chains in the produced 364 samples was investigated by polarized infrared spectroscopy. The acquired polarized ATR-IR spectra were analyzed considering the peak 366 at 2960 cm⁻¹, related to the CH₃ asymmetric stretching, as reference 367 band, since its dichroic ratio is unitary, independently of the polymer's 368 structure [18,19]. In our case, for all samples the dichroic ratios of the 369 peaks at 1367 cm⁻¹ and 837 cm⁻¹ were calculated, since, as previously 370 mentioned, these two peaks are assigned to the CH₃ deformation and 371 the =CH out of plane bending of cis-1,4-polyisoprene, respectively. In 372 fact, the =CH and the -CH₃ bonds lie in two almost perpendicular direc- 373 tions, and they strongly depend on the orientation of the polyisoprene 374 units in the fibers and films [33]. Table 4 summarizes the calculated di- 375 chroic ratios for the analyzed electrospun samples and the calculated dichroic ratios for the solvent cast films are reported, as a reference. As 377 expected, for the cast film these values were approximately one for 378 both peaks and in all configurations. Fig. 10a displays the ATR spectra 379 in the 0° L and 90° L configurations. It is possible to notice that the rela-380 tive intensities of the peaks are comparable. In fact, in the solvent casting technique no direct stress is applied for the formation of the samples 382 and, consequently, the lack of an applied stress during the film forma- 383 tion leads to a random organization of the macromolecular chains in 384 the sample. Concerning the electrospun samples, randomly oriented 385 and aligned fibers showed different trends. The dichroic ratios of the 386 randomly oriented fibrous mats were very similar to those of the sol- 387 vent cast film. On the contrary, the aligned fibers presented high $R_L(0)/388$ 90) and $R_T(0/90)$ values for the peak at 837 cm⁻¹, indicating a preferential orientation of the macromolecular chains. In Fig. 10b the peaks at 390 837 cm⁻¹of the ATR spectra in the $R_L(0/90)$ and $R_T(0/90)$ configurations are compared. The orientation was probably given by the processing technique itself and in particular by the ejection of the solution 393 during the formation of the Taylor cone. It is highly unlikely that the 394 force applied through the rotating drum could have induced the 395

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Table 4Dichroic ratio values of the solvent cast and electrospun samples.

Sample	Sample R _L (0/90)		R _T (0/90)		R ₀ (L/T)	R ₀ (L/T)		R ₉₀ (L/T)	
	1370_cm_ ⁻¹	837_cm_ ⁻¹	1370 _{cm} ⁻¹	837_cm_ ⁻¹	1370 _{cm} ⁻¹	837_cm_ ⁻¹	1370 _{cm} ⁻¹	837_cm_ ⁻¹	
Solvent cast	1.00	1.14	1.10	0.92	1.01	1.03	1.11	0.83	
DR2:ES-F	0.96	0.83	1.06	0.89	0.90	0.97	1.00	1.05	
DR2:ES-R	1.07	1.87	1.34	2.01	1.26	1.36	1.58	1.47	

orientation of the polymer chains, being the collector's speed too slow. The alignment of the macromolecular chains was probably due to the influence of the electrostatic field on the polymer jet, which was able to create elongation strains and shear forces resulting in a high degree of molecular orientation. It was hypothesized that the polymer chains were oriented all in the same direction but are not packed to form a lattice. This reason could explain why the ATR measurements revealed a preferential orientation of the chains in the fiber, whereas the XRD spectra did not show diffraction peaks relative to a lattice organization.

4. Conclusions

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t4.2 t4.3 t4.4 t4.5 t4.6 t4.7

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Natural rubber based fibers were successfully manufactured by electrospinning, for the first time, starting from neat dry rubber solutions and GNPs/dry rubber suspensions. Different dry rubber solution concentrations were tested, in order to select the optimal one (i.e. 2 wt.%). For the hybrid systems, a disagglomeration procedure was developed to obtain a proper dispersion of the filler. Both randomly distributed and aligned fibers were produced using a fixed and rotating collector, respectively. The obtained fibers were uniform, homogeneous, defect-free and characterized by an average diameter of around 1 μm . Results clearly show that the solution/suspension viscosity can be considered the main controlling parameter in the electrospinning process,

in terms of fiber dimension and quality, as expected and validated by 417 a semiempirical equation. In the case of the hybrid fibers, the addition 418 of the filler led to an increment in the suspension viscosity and conduc- 419 tivity. Consequently a slight increase in the fiber diameter (around 420 1.2 µm) was registered and this effect was accompanied by an evident 421 roughening of the fiber surface. The internal fiber structure was also analyzed by X-ray diffraction and attenuated total reflectance experi- 423 ments. The XRD diffraction patterns of the neat and hybrid spun fibers 424 showed that the fibers are amorphous; however interesting results 425 were obtained from the ATR-IR analysis, suggesting an influence of the 426 electrospinning process on the molecular orientation of the natural rub- 427 ber polymer chains. Indeed, significantly higher dichroic ratio values for 428 the aligned fibers were obtained with respect to the randomly oriented 429 ones, as well as to the solvent cast films. Thus the electrospinning pro- 430 cess seemed to induce an orientation of the polymeric chains. Based 431 on these findings, there is space for future works to promote strain in- 432 duced crystallization, stretching the fibers during the spinning stage 433 and using the oriented amorphous areas as nucleation sites. 434

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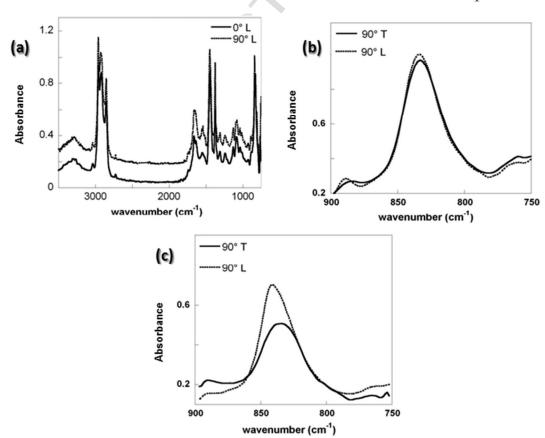


Fig. 10. (a) ATR spectra of the solvent cast film in the 0° L (continuous line) and 90° L (dotted line) configurations. ATR bands centered at 837 cm⁻¹ obtained in the 90° L (dotted line) and 90° T (continuous line) configurations of random neat electrospun fibers (b); and aligned hybrid electrospun fibers (c). All spectra are normalized to the absorbance values at 2960 cm⁻¹.

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